

# Enhancement of oxygen and methane solubility in 1-hexyl-3-methylimidazolium bis(trifluoromethylsulfonyl) imide using carbon dioxide

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The presence of CO<sub>2</sub> increases the solubility of O<sub>2</sub> and CH<sub>4</sub> in 1-hexyl-3-methylimidazolium bis(trifluoromethylsulfonyl) imide at 25 °C and pressures to 13 bar.

Due to their volatile nature and associated contributions to air pollution and human health hazards, there has been an emphasis on the development of new solvents to replace volatile organic chemicals (VOCs). Since ionic liquids (ILs) are non-volatile, they have the potential to displace some VOC solvents. In fact, ILs have been shown to be excellent solvents for a wide range of chemical reactions and separations.<sup>1–3</sup> Numerous homogeneously catalyzed reactions including hydrogenations, oxidations, and hydroformylation reactions have been run effectively in these novel solvent media.<sup>1–6</sup> Moreover, since our publication that CO<sub>2</sub> can be used to extract organic compounds from ILs without contamination of the extracted product,<sup>7,8</sup> several research groups have shown that IL/CO<sub>2</sub> biphasic systems can be even more effective as reaction media.<sup>4–6,9</sup> We and others have shown that CO<sub>2</sub> is very soluble in ILs but that H<sub>2</sub>, O<sub>2</sub> and CO are not.<sup>10–13</sup> Nonetheless, these reactant gases have been used very successfully in the presence of supercritical CO<sub>2</sub> for hydroformylation, hydrogenation, and oxidation reactions.<sup>4–6,9</sup> For instance, the presence of supercritical CO<sub>2</sub> increases the reaction rates for enantioselective hydrogenation of imines in ILs.<sup>4</sup> Increased H<sub>2</sub> solubility in the presence of CO<sub>2</sub> was observed at high pressures when large amounts of CO<sub>2</sub> were used.<sup>4</sup> Therefore, we are interested more generally in how the presence of CO<sub>2</sub> affects the solubility of lower solubility gases in ILs both at high pressures and at more moderate pressures, as will be presented here. Specifically, in this communication, we present the results for the solubility of O<sub>2</sub>/CO<sub>2</sub> and CH<sub>4</sub>/CO<sub>2</sub> mixtures in 1-hexyl-3-methylimidazolium bis(trifluoromethylsulfonyl) imide ([hmim][Tf<sub>2</sub>N]) at 25 °C in a pressure range of 1 to 13 bar. These results are the first to show that the solubility of O<sub>2</sub> and CH<sub>4</sub> in ILs can be dramatically enhanced with small amounts (and low pressures) of CO<sub>2</sub>.

[hmim][Tf<sub>2</sub>N] was synthesized in our laboratory according to the published procedures.<sup>10</sup> The IL was dried at 70 °C under high vacuum before use and the water content in the IL was found to be ~160 ppm using Karl-Fischer titration. Coleman instrument grade CO<sub>2</sub>, CH<sub>4</sub>, CH<sub>4</sub>/CO<sub>2</sub>, and O<sub>2</sub>/CO<sub>2</sub> gas mixtures were purchased from Mittler Supply, Inc. The solubility of pure CO<sub>2</sub>, CH<sub>4</sub> and O<sub>2</sub> in [hmim][Tf<sub>2</sub>N] at 25 °C was measured in an

Intelligent Gravimetric Analyzer (Hiden Analytical Limited, England), the details of which are given elsewhere.<sup>12</sup> The solubility of gas mixtures in [hmim][Tf<sub>2</sub>N] at 25 °C was measured in a constant volume view cell and a Varian 3400CX gas chromatograph was used for online measurement of the vapor phase composition. A Heise pressure gauge was used for pressure measurement and the volumes of the cell and the lines were calibrated accurately. In a typical experiment, the cell was loaded with a known amount of sample and was evacuated at 70 °C to remove any dissolved gases. Then the cell was loaded with the feed gas to an initial pressure and the vapor phase was sampled immediately to determine the composition of the feed gas. Then the sample was stirred until equilibrium was attained, as indicated by no further drop in pressure. The final liquid volume and the pressure were measured and the vapor phase was sampled to determine the vapor phase composition. The liquid phase composition was calculated from the difference in the initial and final number of moles of each component in the vapor phase. The moles and fugacity of each component were calculated using the Virial equation of state.<sup>14</sup> Experiments were repeated at several pressures between 1 and 13 bar.

The solubility of pure CO<sub>2</sub>, CH<sub>4</sub> and O<sub>2</sub> in [hmim][Tf<sub>2</sub>N] at 25 °C is shown in Fig. 1. The solubility of all three gases increases with an increase in pressure and CO<sub>2</sub> was found to be the most soluble gas. These trends were consistent with those reported by our group for the solubility of these gases in other ILs.<sup>12</sup> The low solubility of oxygen in ILs has several implications for performing oxidation reactions. For example, the low solubility of oxygen in

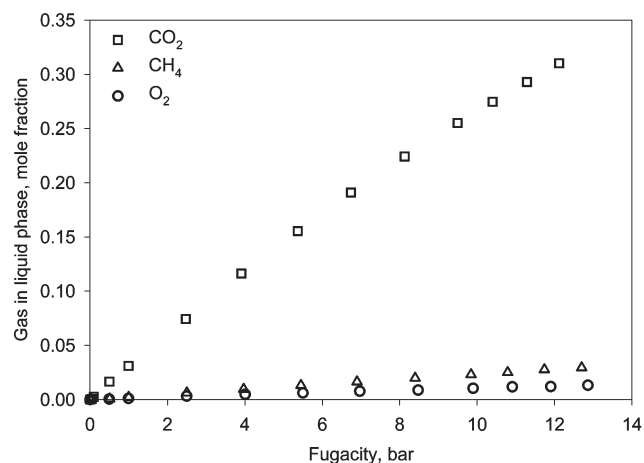


Fig. 1 Solubility of gases in [hmim][Tf<sub>2</sub>N] at 25 °C.

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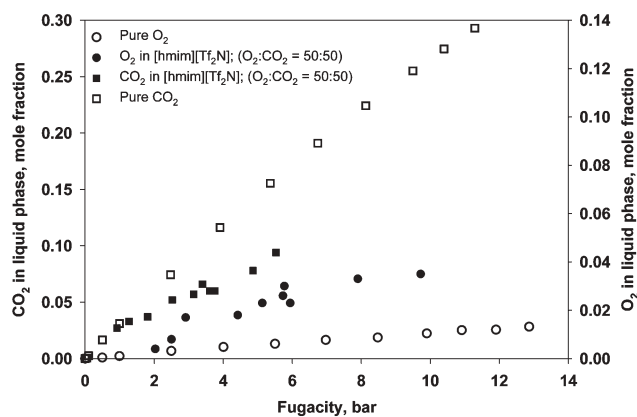


Fig. 2 Solubility of O<sub>2</sub> in [hmim][Tf<sub>2</sub>N] at 25 °C in the presence of CO<sub>2</sub>. Feed gas composition: O<sub>2</sub>/CO<sub>2</sub> = 50/50.

ILs may lower reaction rates, decrease product yields and cause the reaction to be mass-transfer limited. One can overcome this limitation by increasing the oxygen pressure but this may result in safety concerns.

The solubility of oxygen in [hmim][Tf<sub>2</sub>N] at 25 °C in the presence of CO<sub>2</sub> is shown in Fig. 2 and Table 1. In the figure, oxygen solubility is given on the right axis with CO<sub>2</sub> solubility indicated on the left axis. The solubility of each component in the gas mixture is compared with the pure gas solubility at the same fugacity. Fugacity,  $f_i$ , is defined as  $f_i = y_i \phi_i P$ , where  $y_i$  is the mole fraction,  $P$  is the pressure and  $\phi_i$  is the fugacity coefficient, which corrects for vapor phase nonidealities. Here we use the Virial equation of state to calculate  $f_i$  for both pure ( $y_i = 1$ ) gases and components in the mixed gas system. The fugacity coefficients are very close to unity for O<sub>2</sub> but range between 0.94 and 1.0 for CO<sub>2</sub>. CO<sub>2</sub> solubility is less than the pure gas solubility at all pressures (*i.e.*, fugacities). For example, the solubility at a CO<sub>2</sub> fugacity of 4 bar decreases from 0.12 mole fraction for the pure gas to about 0.07 mole fraction in the mixed gas system. On the other hand, the solubility of oxygen increased substantially compared to the pure gas solubility at all pressures. For instance, with the presence of CO<sub>2</sub> in the liquid phase the oxygen solubility increased from 0.006 mole fraction to 0.03 mole fraction at an O<sub>2</sub> fugacity of 5.7 bar. This is shown in Table 1 in terms of the enhancement factor (EF), which is defined as oxygen solubility in the mixed gas system divided by the oxygen solubility in the pure O<sub>2</sub> system, at the same

Table 1 Vapor–liquid equilibrium for CO<sub>2</sub> (1)–O<sub>2</sub> (2)–[hmim][Tf<sub>2</sub>N] (3) at 25 °C

$P^{\text{total}}$ bar	Liquid phase composition			Vapor phase composition		$f_{\text{CO}_2}$ bar	$f_{\text{O}_2}$ bar	$x_{\text{O}_2}$ , pure gas mole fr.	EF
	$x_1$	$x_2$	$x_3$	$y_1$	$y_2$				
3.0	0.03	0.004	0.96	0.31	0.69	0.90	2.0	0.002	1.7
3.8	0.03	0.008	0.96	0.34	0.66	1.3	2.5	0.003	3.0
4.8	0.04	0.02	0.95	0.39	0.61	1.8	2.9	0.003	5.7
7.0	0.05	0.02	0.93	0.37	0.63	2.5	4.4	0.005	3.8
8.4	0.06	0.02	0.92	0.39	0.61	3.1	5.1	0.005	4.3
9.5	0.06	0.03	0.91	0.40	0.60	3.6	5.7	0.006	4.4
9.5	0.07	0.02	0.91	0.37	0.63	3.4	5.9	0.006	3.7
9.7	0.06	0.03	0.91	0.40	0.60	3.8	5.8	0.006	4.9
13.1	0.08	0.03	0.89	0.39	0.61	4.9	7.9	0.008	4.0
15.7	0.09	0.04	0.87	0.38	0.62	5.5	9.7	0.010	3.5

O<sub>2</sub> fugacity. To aid in these calculations, we give the O<sub>2</sub> solubility (second column from right) if it were a pure gas at the same oxygen fugacity as is present in the mixture (third column from right). The EFs range from 1.7 to 4.9 for the CO<sub>2</sub>/O<sub>2</sub>/[hmim][Tf<sub>2</sub>N] system. Of course, the total pressure when using gas mixtures would be greater than the pressure of pure gas. For example, at an oxygen fugacity of 5.7 bar the total pressure, due to the presence of CO<sub>2</sub>, is 9.5 bar for a feed gas with an initial composition of about 50/50 O<sub>2</sub> to CO<sub>2</sub> ratio. However, even if one applied 9.5 bar of pure O<sub>2</sub>, the solubility of the O<sub>2</sub> would only be about 0.01 mole fraction. This is less than the O<sub>2</sub> solubility at a total pressure of 9.5 bar, where the initial gas mixture is about half O<sub>2</sub> and half CO<sub>2</sub>. These comparisons can be made easily by examination of the data in Table 1. Thus, at a given total pressure the O<sub>2</sub> solubility is enhanced with the O<sub>2</sub>/CO<sub>2</sub> mixture, even though the gas phase is “diluted” with CO<sub>2</sub>.

As shown in Fig. 1, the solubility of methane in [hmim][Tf<sub>2</sub>N] is substantially less than the solubility of CO<sub>2</sub>. These results suggest that ILs could be used for separating methane from CO<sub>2</sub>.<sup>12</sup> Here we present the solubility of methane in [hmim][Tf<sub>2</sub>N] in the presence of CO<sub>2</sub> at 25 °C using two different gas mixtures, *viz.*, about 90/10 and 50/50 CH<sub>4</sub> to CO<sub>2</sub> mole ratios. The solubility of the gas mixture is compared with the pure gas solubility of each component in Fig. 3 and in Table 2. Once again the partial pressure of each component in the vapor phase was corrected for nonideality using the Virial equation of state. As with the O<sub>2</sub>/CO<sub>2</sub> gas mixture, the solubility of CO<sub>2</sub> decreases compared to the pure gas solubility at all pressures. Methane solubility in the presence of CO<sub>2</sub> increased at all pressures. With the pure gas, the solubility of methane in [hmim][Tf<sub>2</sub>N] is 0.03 at a pressure of 13 bar. Interestingly, similar solubilities of methane can be obtained at a methane fugacity of just ~5.7 bar using a 50/50 CH<sub>4</sub>/CO<sub>2</sub> gas mixture and at a methane fugacity of ~8.5 bar when a 90/10 CH<sub>4</sub>/CO<sub>2</sub> gas mixture was used. The important result is that a small amount of CO<sub>2</sub> increases the CH<sub>4</sub> solubility. For the 90/10 CH<sub>4</sub>/CO<sub>2</sub> gas mixture with a methane fugacity of ~8.5 bar the CO<sub>2</sub> concentration in the liquid phase is only 0.01 mole fraction, yet the methane solubility is enhanced to 0.03 mole fraction, which is much greater than the solubility of pure methane at 13 bar, a substantially higher pressure. Note from the data in Table 2 that the enhancement factors for methane are generally lower than those observed for oxygen. Nevertheless, CO<sub>2</sub> does

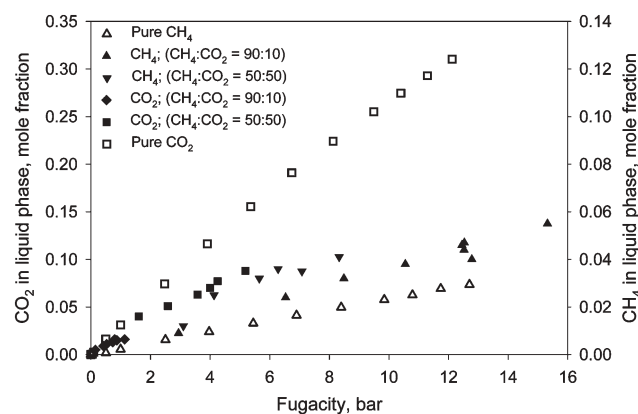


Fig. 3 Solubility of CH<sub>4</sub> in [hmim][Tf<sub>2</sub>N] at 25 °C in the presence of CO<sub>2</sub>. Feed gas composition: CH<sub>4</sub>/CO<sub>2</sub> = 50/50 and CH<sub>4</sub>/CO<sub>2</sub> = 90/10.

**Table 2** Vapor–liquid equilibrium for CO<sub>2</sub> (1)–CH<sub>4</sub> (2)–[hmim][Tf<sub>2</sub>N] (3) at 25 °C

$p_{\text{total}}$ bar	Liquid phase composition			Vapor phase composition		$f_{\text{CO}_2}$ bar	$f_{\text{CH}_4}$ bar	$x_{\text{CH}_4}$ , pure gas mole fr.	EF
	$x_1$	$x_2$	$x_3$	$y_1$	$y_2$				
3.1	0.005	0.009	0.99	0.05	0.95	0.15	2.9	0.007	1.4
7.0	0.009	0.02	0.97	0.06	0.94	0.4	6.5	0.02	1.6
9.2	0.01	0.03	0.96	0.06	0.94	0.5	8.5	0.02	1.6
11.5	0.01	0.04	0.95	0.07	0.93	0.7	10.6	0.02	1.6
13.7	0.02	0.05	0.94	0.07	0.93	0.9	12.5	0.03	1.6
13.7	0.02	0.04	0.94	0.07	0.93	0.9	12.5	0.03	1.5
13.7	0.02	0.05	0.94	0.07	0.93	0.9	12.5	0.03	1.6
13.9	0.02	0.04	0.94	0.06	0.94	0.8	12.8	0.03	1.4
17.0	0.02	0.06	0.93	0.07	0.93	1.1	15.3	0.04	1.6
4.8	0.04	0.01	0.95	0.35	0.66	1.6	3.1	0.007	1.8
6.8	0.05	0.03	0.92	0.39	0.61	2.8	4.1	0.01	2.6
9.5	0.06	0.03	0.91	0.39	0.61	3.8	5.6	0.01	2.5
10.6	0.07	0.04	0.90	0.4	0.60	4.0	6.3	0.01	2.5
11.7	0.08	0.04	0.89	0.38	0.61	4.3	7.1	0.02	2.1
14.0	0.09	0.04	0.87	0.39	0.61	5.2	8.3	0.02	2.1

substantially enhance CH<sub>4</sub> solubility in [hmim][Tf<sub>2</sub>N], even at relatively low pressures and concentrations. The implication of this result is that the efficiency of separating CO<sub>2</sub> from methane using ILs may be low and may require additional stages to achieve the desired separation.

These results, decreased solubility of CO<sub>2</sub> relative to the pure gas and increased solubility of O<sub>2</sub> or CH<sub>4</sub> relative to the pure gas, indicate that gas solubility in ionic liquids cannot be described by a regular solution theory (RST) model, as has been suggested by other researchers.<sup>15</sup> For a binary system RST predicts higher solubility when the solubility parameters of the solute and the solvent are more similar. Assuming that the energies of vaporization of most ILs are similar (and large) then ILs with larger molar volumes will have smaller solubility parameters and, thus, more readily dissolve a gas like CO<sub>2</sub>, which has a relatively small solubility parameter. This trend does seem to be borne out experimentally for CO<sub>2</sub> solubility in various ILs.<sup>15</sup> However, RST for the ternary mixture would predict that the solubility of both the lower solubility gas (O<sub>2</sub> or CH<sub>4</sub>) and the CO<sub>2</sub> should increase. This is not what was observed in this study and, thus, these results cannot be explained by RST. Reduction of the solubility of one or more gases in the mixed gas system compared to the pure gas systems is common with solid adsorbents. There is a competition for adsorption sites by the two gases. A crude extension of this concept to gas solubility in ILs would mean that CO<sub>2</sub>, which has been shown to interact strongly with the anion,<sup>16</sup> increases the solubility of the O<sub>2</sub> or the CH<sub>4</sub> through dispersion forces. However, the presence of the O<sub>2</sub> or the CH<sub>4</sub> then takes up some of sites around the anion, thus reducing the solubility of the CO<sub>2</sub> relative to the pure gas. Of course, this is pure speculation and more experiments, modeling and simulations are necessary to fully understand these mixed gas systems.

In this work we have shown that CO<sub>2</sub> can dramatically enhance the solubility of O<sub>2</sub> and CH<sub>4</sub> in [hmim][Tf<sub>2</sub>N]. While this makes some gas separations with ILs more challenging, it also provides an easy method to increase the solubility of some low solubility reactant gases. These results suggest that small amounts of CO<sub>2</sub>

could be used to enhance the solubility of paraffins and other nonpolar compounds in ILs, as well.

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